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(54) Title: SURFACE MODIFIED SURGICAL INSTRUMENTS, DEVICES, IMPLANTS, CONTACT LENSES AND THE LIKE (57) Abstract Improved medical devices and instruments prepared by an improved method of producing hydrophilic, gamma-irradiation or electron beam-irradiation induced polymerized and chemically grafted coatings or plastic surfaces of articles adapted for contacting living tissue, the improvement comprising carrying out the graft polymerisation in an aqueous solution under specific combinations of the following conditions: 1) monomer concentration in the range of from about 0.1 % to about 50 % by weight; 2) total gamma or electron beam irradiation dose in the range of from about 0.001 to less than about 0.50 Mrad; and 3) gamma dose rate in the range of from about 10 to about 2500 rads/min or electron beam-irradiation dose rate in the range of from about 10 to about 10 ⁸ rads/min.		

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**SURFACE MODIFIED SURGICAL INSTRUMENTS,
DEVICES, IMPLANTS, CONTACT LENSES AND THE LIKE**

BACKGROUND OF THE INVENTION

Related Applications

This application is a continuation-in-part of application Serial No. 304,479, filed February 1, 1989,
5 which is a continuation-in-part of application Serial No. 037,153, filed April 10, 1987, now U.S. Patent No. 4,806,382, issued February 21, 1989.

Field of the Invention

10 The present invention relates to plastic surgical instruments, medical devices, prosthetic cardiovascular implants and implants for hard and soft tissue, contact lenses and the like and methods for improving surfaces thereof.

Prior Art

15 Studies have shown that the surgical implantation of ocular implants such as intraocular lenses (IOL), etc., can result in the loss of significant corneal endothelial tissue unless great care is taken to ensure a lack of contact between the device and the endo-
20 thelium. Most ocular implants are constructed of hydrophobic polymethylmethacrylate (PMMA) polymers because of their superior optical qualities, resistance to biodegradation, etc. It has been found, however, that PMMA surfaces adhere to endothelial cells upon
25 even casual contact and that separation of the surface therefrom results in a tearing away of the endothelial tissue adhered to the polymer surface. Similar adhesive interactions with other ocular tissues, i.e., the iris, can also cause adverse tissue damage. Other
30 hydrophobic polymers which are used or have been

proposed for use in ocular implants (i.e., polypropylene, polyvinylidene fluoride, polycarbonate, polysiloxane) also can adhere to ocular tissue and thereby promote tissue damage.

5 It is well documented in the prior art that a significant disadvantage inherent in PMMA IOLs resides in the fact that any brief, non-traumatic contact between corneal endothelium and PMMA surfaces results in extensive damage to the endothelium. See Bourne et
10 al, Am. J. Ophthalmol., Vol. 81, pp. 482-485 (1976); Forster et al, Trans. Am. Acad. Ophthalmol. Otolaryngol., Vol. 83, OP-195-OP-203 (1977); Katz et al, Trans. Am. Acad. Ophthalmol. Otolaryngol., Vol. 83, OP-204-OP-212 (1977); Kaufman et al, Science, Vol. 198,
15 pp. 525-527 (1977) and Sugar et al, Arch. Ophthalmol., Vol. 96, pp. 449-450 (1978) for a discussion of the problem associated with implant surface/endothelium contact.

 Since it is extremely difficult to avoid any
20 contact between implant surfaces and endothelium during surgical procedures and especially to other sensitive ocular tissues during implant life, i.e., the iris, ciliary sulcus, etc., efforts have been undertaken to modify the PMMA ocular implant surfaces to reduce the
25 tendency thereof to adhere to and damage corneal endothelium.

 Ocular implant surfaces have been coated with various hydrophilic polymer solutions or temporary soluble coatings such as methylcellulose, polyvinylpyrrolidone (Katz et al and Knight et al, supra), etc.,
30 to reduce the degree of adhesion between the implant surfaces and tissue cells. While offering some temporary protection, these methods have not proven entirely satisfactory since such coatings complicate
35 surgery, do not adhere adequately to the implant

surfaces, become dislodged or deteriorate after implantation, dissolve away rapidly during or soon after surgery or may produce adverse post-operative complications. Moreover, it is difficult to control the thicknesses and uniformity of such coatings.

Yalon et al [Acta: XXIV, International Congress of Ophthalmology, ed. Paul Henkind (1983)] and Knight et al [Chem. Abs., Vol. 92: 203547f (1980)] have reported attempts to produce protective coatings on PMMA implant surfaces by gamma-radiation induced polymerization of vinylpyrrolidone thereon. Their efforts were not altogether successful, however, since their methods also presented problems in controlling the optical and tissue protective qualities of the coatings. Process conditions and parameters (i.e., monomer concentration solvent, dose and dose rate) were not specified. The resulting coatings were of poor quality and non-uniform mechanical stability.

In U.S. Patent No. 4,806,382, issued February 21, 1989, there are described improved methods for producing hydrophilic, gamma irradiation induced polymerized and chemically grafted coatings on ocular implants constructed of a variety of polymeric materials, which methods overcome the above-noted difficulties and disadvantages.

The invention described in that patent is predicated on the discovery of certain process conditions and parameters that produce thin hydrophilic gamma irradiation induced polymerized and chemically grafted coatings of N-vinylpyrrolidone (NVP) [PVP], copolymerized NVP and 2-hydroxyethylmethacrylate (HEMA) [P(NVP-HEMA)], or HEMA [PHEMA] and their copolymers, particularly with ionic comonomers on the surfaces of ocular implants constructed of materials including polymethylmethacrylate (PMMA) and of other process

conditions and parameters which produce thin gamma irradiation induced graft PVP, P(NVP-HEMA), PHEMA or copolymer coatings on the surfaces of ocular implant articles constructed of materials including polypropylene (PP), polyvinylidene fluoride (PVDF), polycarbonate (PC) and polysiloxane or silicone (PSi). The coatings increase the hydrophilicity of the implant surface and minimize adhesion between the surface and sensitive ocular tissues such as corneal endothelium or iris thereby minimizing tissue damage and post-operative complications occasioned by contact between the implant surface and ocular tissue. The coatings produced by the improved method of the invention described in U.S. Patent No. 4,806,382 are thin and uniform. Moreover, they are chemically bound to the surface of the ocular implant and, therefore, far more durable and less subject to removal, degradation or deterioration during or following surgery than the coatings produced by prior art methods.

The improved gamma-irradiation induced graft polymerization of NVP, HEMA or mixtures of NVP and HEMA on ocular implant surfaces comprising PMMA to form optimum PVP, P(NVP-HEMA) or PHEMA graft polymer surface modifications thereon described in U.S. Patent No. 4,806,382 comprises carrying out the graft polymerization in an aqueous solution under specific combinations of the following conditions:

- a) monomer concentration in the range of from about 0.5 to about 50%, by weight;
- b) total gamma dose in the range of from about 0.01 to about 0.50 Mrad;
- c) gamma dose rate in the range of from about 10 to about 2500 rads/minute; and

d) maintaining the molecular weight of the polymer in solution in the range of from about 250,000 to about 5,000,000.

The maintenance of the molecular weight of the polymer in solution at certain values, identified in U.S. Patent No. 4,806,382 as a critical condition of the method is not actually a "condition" of the method, but rather, as stated in the specification, a result which is dependent on the reaction conditions employed in carrying out the graft polymerization process. It is, therefore, not appropriate to specify the molecular weight of the polymer in solution as a process "condition" since it is rather an outcome of the reaction conditions used in this invention and may be widely varied depending on specific gamma graft monomer-substrate-process conditions. If a certain set of fixed conditions are employed, namely: monomer, monomer concentration, total gamma dose and gamma dose rate, the molecular weight of the polymer formed in solution cannot be independently varied, but will be an output of the process which is dependent upon the values of the above-noted monomer concentration, total gamma dose and gamma dose rate conditions. For example, in the presence of certain ionic monomers, solvents or radical inhibitors, solution polymerization may be inhibited significantly without sacrificing efficient surface graft polymerization and the resulting solution polymer molecular weight may thereby be relatively low (i.e., as low as 5,000 - 10,000).

Since the application which matured into U.S. Patent No. 4,806,382 was filed, the inventors of the subject matter defined therein conducted additional research and unexpectedly found that although relatively low doses of 0.01 to 0.20 Mrad are generally preferred for the compositions of this invention, the

process could be conducted at a total gamma dose as low as 0.001 Mrad.

The state of the art prior to the application which matured into U.S. Patent No. 4,806,382 taught the use of relatively high gamma doses, generally greater than 0.5 Mrad, for gamma polymerization grafting, and it was therefore surprising to find that surface grafting could be achieved at doses as low as 0.01 Mrad. The achievement of effective grafting at doses as low as 0.001 Mrad is consequently an even more unexpected result of the process of this invention. Furthermore, although grafting with monomer concentrations as low as 0.5 wt% was indicated in prior U.S. Patent No. 4,806,382, further research has revealed that monomer concentrations as low as 0.1 wt% may be utilized in some embodiments of the graft process of this invention.

Optimally, the method may also be carried out under one or more of the following conditions:

- e) substantially excluding free oxygen from the aqueous graft polymerization solution;
- f) maintaining the thickness of the PVP or P(NVP-HEMA) surface graft in the range of from about 100 Å to about 150 microns;
- g) including a free radical scavenger in the aqueous graft polymerization solution; and
- h) including in the aqueous graft polymerization solution a swelling solvent for PMMA or other polymer substrate surface.

The improved gamma-irradiation induced graft polymerization of NVP, mixtures of NVP and HEMA or HEMA on ocular implant surfaces comprising PP, PVDF, PC or PSi to form optimum PVP or P(NVP-HEMA) surface grafts thereon may also be carried out under specific combinations of the process parameters as indicated

above for PMMA but also under conditions which involve excluding free oxygen from the polymerization solution for preferred surface modification of these ocular implant polymer substrates.

5 At the present time, surgical instruments, medical devices, prosthetic implants, contact lenses and the like which are intended for contact with blood or with sensitive tissue surfaces are constructed of materials having the necessary physical properties to enable
10 their use for the intended application; however, they suffer from the disadvantage that due to the generally hydrophobic nature of the blood or tissue contacting surfaces thereof, they exhibit undesired thrombogenic properties and significant damage is done to fragile or
15 sensitive tissues by adhesion and manipulation or movement on contact with these instruments.

 In copending application Serial No. 304,479, filed February 1, 1989, there are described improved methods for producing hydrophilic, gamma irradiation induced
20 polymerized and chemically grafted coatings on such instruments, devices and the like so constructed of a variety of polymeric materials.

 The invention described in that application is predicated on the discovery of certain process
25 conditions and parameters that produce thin, hydrophilic, gamma irradiation polymerized and chemically grafted coatings of N-vinylpyrrolidone (NVP [PVP]), copolymerized NVP and 2-hydroxyethylmethacrylate (HEMA) [P(NVP-HEMA)] or HEMA [PHEMA] on the surfaces of
30 articles adapted for contact with living tissue of a human or non-human animal, e.g., surgical instruments, medical devices, prosthetic implants, contact lenses and the like constructed of a wide variety of plastic materials. For purposes of the following description

of the invention, the term "tissue" is intended to include blood as well as solid tissue surfaces.

5 The surface modifications or chemically grafted coatings of the invention increase the hydrophilicity of the article surfaces and minimize adhesion between the surface and sensitive tissues such as blood cells, vascular endothelium, peritoneum, pericardium, etc., thereby minimizing tissue damage and complications occasioned by contact between the article and such
10 tissues. The coatings produced are thin and reproducibly uniform. Moreover, they are chemically bound to the surface of the article and, therefore, are far more durable and less subject to removal, degradation or deterioration during or following utilization of the
15 articles than the coatings produced by prior art methods.

It is an object of the present invention to provide still further improved method for producing permanent, thin, uniform, tissue-protective hydrophilic surface
20 modifications of plastic surgical instruments, medical devices, prosthetic implants, contact lenses and the like.

It is a further object of the invention to provide plastic surgical instruments, medical devices,
25 prosthetic implants, contact lenses and the like having improved blood compatible and tissue-protective surface modifications thereon.

SUMMARY OF THE INVENTION

The present invention is predicated on the
30 discovery of certain process conditions and parameters that produce thin, hydrophilic, gamma irradiation polymerized and chemically grafted coatings of N-vinylpyrrolidone (NVP [PVP]), copolymerized NVP and 2-hydroxyethylmethacrylate (HEMA) [P(NVP-HEMA)] or HEMA

[PHEMA] on the surfaces of articles adapted for contact with living tissue of a human or non-human animal, e.g., surgical instruments, medical devices, prosthetic implants, contact lenses and the like constructed of a wide variety of plastic materials. For purposes of the following description of the invention, the term "tissue" is intended to include blood as well as solid tissue surfaces.

The surface modifications or chemically grafted coatings of this invention increase the hydrophilicity of the article surfaces and minimize adhesion between the surface and sensitive tissues such as blood cells, vascular endothelium, peritoneum, pericardium, etc., thereby minimizing tissue damage and complications occasioned by contact between the article and such tissues. The coatings produced are thin and reproducibly uniform. Moreover, they are chemically bound to the surface of the article and, therefore, are far more durable and less subject to removal, degradation or deterioration during or following utilization of the articles than the coatings produced by prior art methods.

The present invention relates to an improved method for modifying a plastic surface of an article, the surface adapted for contact with living tissue of a human or non-human animal, by the gamma-irradiation induced polymerized chemically grafted coating thereon of:

- 1) a monomer comprising N-vinylpyrrolidone (NVP),
- 2) a monomer comprising 2-hydroxyethylmethacrylate (HEMA),
- 3) a mixture of (NVP) and (HEMA), (NVP-HEMA), or
- 4) a mixture of 1), 2) or 3) with up to about 50 wt%, based on the total monomer weight, of an ionic

10

monomer, salt of an ionic monomer or mixture thereof;
so as to form a hydrophilic graft polymer coating of:

I. polyvinylpyrrolidone (PVP),

II. poly-2-hydroxyethylmethacrylate (HEMA),

5 III. a copolymer of (NVP) and (HEMA), [P(NVP-
HEMA)], or

IV. a copolymer of (NVP), (HEMA) or (NVP-HEMA) and
said ionic monomer, on said surface, the improvement
comprising:

10 conducting the gamma-irradiation induced graft
polymerization in an aqueous solution under the
following conditions:

a) monomer concentration in the range of
from about 0.1% to about 50%, by weight;

15 b) total gamma dose in the range of from
about 0.001 to less than about 0.50 Mrad; and

c) gamma dose rate in the range of from
about 10 to about 2500 rads/min.

Optimally, the method may also be carried out as
20 described above and, additionally, under one or more of
the following conditions:

d) substantially excluding free oxygen from
the graft polymerization solution;

25 e) maintaining the thickness of the polymer
coating in the range of from about 100 Å to about 100
microns;

f) including a free radical scavenger in the
aqueous graft polymerization solution; and

30 g) including in said aqueous graft polymeri-
zation solution a swelling solvent for the plastic
surface.

Alternatively, the coating may be graft polymerized
on the plastic surface utilizing electron beam
irradiation.

The invention also relates to articles produced according to the above-described method.

DETAILED DESCRIPTION OF THE INVENTION

The entire disclosure of U.S. Patent No. 4,806,382 is incorporated herein by reference.

Yalon et al (supra) and Knight et al (supra) disclose gamma-irradiation coatings on PMMA using N-vinylpyrrolidone (NVP) and 2-hydroxyethylmethacrylate (HEMA) and indicate poor dynamic (abrasive) protection of endothelium for these coatings. Dissolvable coatings of polyvinyl-alcohol (PVA) were regarded as optimal for intraocular lenses (IOLs) by Knight et al, supra, and commercial development of a PVA-coated IOL was attempted with unsatisfactory clinical results. The gamma polymerization surface modifications reported were carried out under process conditions of monomer concentration, solvent, dose and dose rate which were not specified and which apparently yielded poor quality, readily abraded coatings. Conditions for producing useful permanent PVP or PHEMA coatings on PMMA IOLs or any other plastic surface are not taught in the prior art. Neither Knight et al, Yalon et al or the literature on gamma-graft polymerization of the past 30 years suggest the process conditions required to achieve the complicated requirements for useful coatings on plastics. These requirements include:

a) Thin, permanent, optically clear (in the case of contact lenses) and uniform graft coatings. The literature generally discloses conditions which produce distortion and degradation of the substrate due to the use of high gamma-radiation dose (>1 Mrad) and non-aqueous solvent media, and yield thick, cloudy, non-uniform coatings (e.g., Chapiro, Radiation Chemistry of Polymeric Systems, John Wiley and Sons, Inc., New York,

1962; Henglein et al, Angew. Chem., Vol. 15, p. 461 (1958).

b) Long-term biocompatibility in vivo.

5 c) Low contact angle (high wettability) for water or underwater air bubble (less than about 30°).

d) Non-adherent to tissue (adhesive force to endothelium less than about 150 mg/cm²).

e) Non-damaging to endothelium (less than ca. 20% damage for in vitro contact tests).

10 f) Measurable graft coating by ESCA or FTIR analysis.

g) Abrasion resistance by sliding (dynamic) friction testing showing no change in wetting (contact angle) and confirming before and after presence of graft coating.

15 h) Rapid hydration - change from dry state to wetted lubricous state on immersion in water (within five minutes).

Yalon et al (supra) disclose an in vitro technique for measuring endothelium damage. Results for PMMA were used to illustrate the method. Although it was noted that FVP coatings reduced cell damage with less damage at higher monomer concentrations, the conditions for the experiment (i.e., irradiation dose, dose rate, etc.) were not disclosed nor were any of the critical process-product relationships indicated.

20 The improved process conditions and parameters of the invention described in U.S. Application Serial No. 304,479 which are necessary to produce useful polymers having a surface modified by gamma-irradiation induced graft polymerization therein of FVP, P(NVP-HEMA) or PHEMA include: % monomer, gamma dose, dose rate, penetration time or swelling time of monomer into the substrate prior to polymerization, and oxygen (air) 30 degassing. Other optimal process conditions include 35

catalysts, free radical scavengers, polymer swelling solvents and temperature. The solution polymer molecular weight and M.W. distribution, the % conversion and residual monomer, the graft polymer thickness and surface properties, etc., are process results which can change markedly as the process variables change. For example, the surface modification achieved for PVP on polymer surfaces will be different when using 10% monomer and 0.1 Mrad if prepared at low dose rates since low dose rates (slower polymerization) favor higher molecular weights. Similarly, degassed oxygen-free reaction media result in improved grafts at much lower doses. The presence of free radical scavengers such as copper or iron salts or organic reducing agents (i.e., ascorbic acid) also greatly influences other process parameters, generally reducing solution polymer molecular weight and preventing solution gelation at high monomer concentrations.

The method of the invention is applicable for the surface modification of medical instruments, devices, implants and contact lenses formed from a variety of plastic materials including, for example, polyacrylates and -methacrylates (i.e., polymethylmethacrylate, polyethylacrylate, polybutyl methacrylate, etc.); polyolefins (polyethylene, polypropylene, polybutadiene); SBS (styrene-butadiene), ethylene-propylene copolymers; SE/BS (styrene-ethylene/-butadiene), polycarbonates (PC) fluorocarbon polymers (i.e., polyvinylidene fluoride-FVDF, polytetrafluoroethylene-PTFE, polyperfluoroethylenepropylene-FEP), polysiloxanes, various aliphatic and aromatic polyurethanes, including polyurethane polyester or polyether block copolymers, polyvinylchloride and various polyesters including dacron PET.

Any instrument, device, implant, etc. constructed of one or more of the above materials may be surface modified according to the present invention to improve the tissue contacting characteristics of the surfaces thereof.

Plastic surgical instruments and implements such as probes, retractors, tissue and vessel separators, irrigation and aspiration tools, phacoemulsification tools, sponges, clamps, gloves, lens glides, positioning tools, forceps, insertion tools, staples, sutures, etc., may be treated in accordance with the present invention.

Medical devices such as hard and soft contact lenses, intravenous and central venous catheters, laser and balloon angioplasty devices, vascular and heart devices (tubes, catheters, balloons, ventricular assists), blood dialysis components, blood oxygenators, ureteral/urinary devices (Foley catheters, stents, tubes and balloons), airway catheters (endotracheal and tracheostomy tubes and cuffs), enteral feeding tubes, wound drainage tubes, blood bags and blood tubing may also be beneficially treated in accordance with the method of the present invention.

Implants which may be modified according to the present invention include, for example, vascular grafts, soft and hard tissue prostheses (mammary, cranio/facial, tendons, joints), heart valves and artificial hearts.

Modification of these instruments, devices, implants, etc. improve the surfaces thereof so as to improve blood compatibility and reduce tissue adhesion and tissue damage during surgical contact and manipulation. Moreover, the invention operates to reduce cell adhesion for reduced inflammation, reduce fibrous capsule formation for soft tissue implants, and reduce

thrombogenicity for cardiovascular devices and prostheses. The invention also acts to reduce bacterial adhesion and thereby reduce the incidence of infection and further operates to reduce interfacial abrasion and friction which is of special value for joint and tendon prostheses.

Polyolefins and polyolefin/hydrocarbon block polymers are useful for constructing medical tubing, catheters, blood bags, sutures, etc. Copolymers of the SBS, EP or SE/BS type may be thermoplastic elastomers which combine rubbery properties with extrudable or injection moldable processing properties. Surface modification of such materials according to the present invention is effective in changing the normal surface characteristics of these polymers from hydrophobic to hydrophilic.

The fluorocarbon polymers are widely used for catheters (i.e., intravenous catheters), for vascular prostheses (i.e., vascular grafts) and for coating medical devices, instruments and implants due to their biocompatibility and inertness. However, the surface properties may be improved significantly according to the present invention to reduce cell and tissue adhesion, and improve blood compatibility.

The silicone polymers are widely used for medical tubing and catheters, for mammary implants and other soft tissue prostheses. Hydrophilic surface modification, according to this invention, acts to reduce cell and tissue abrasion and adhesion and to thereby reduce fibrous capsule formation which is a major complication of soft tissue implants. Similarly, polyvinylchloride surface modification to produce more hydrophilic vinyl tubing and film surfaces can reduce thrombogenicity and improve biocompatibility of blood tubing, blood bags,

catheters and other medical devices made of polyvinyl-chloride.

Polyurethanes which are used for such applications as pacer leads, intravenous catheters, enteral feeding
5 tubes, vascular grafts, etc., are also beneficially modified by the process and materials of this invention to produce more hydrophilic surfaces and make such devices more biocompatible.

Each of the above-described process conditions and
10 parameters of the method of the invention may be varied within the ranges discussed below to produce certain specific combinations which are particularly advantageous for the surface modification of a particular polymeric surface.

15 (a) Monomer concentration: Increasing monomer concentration increases polymer mol. wt. in the graft solution and reduces contact angle (C.A.), i.e., renders the surface more hydrophilic. For example, in the case of forming PVP coatings on PMMA, in the range
20 of from about 3-15% NVP the PVP viscosity mol. wt. (M_v) increases from 560,000 to 2,700,000 and the PMMA graft C.A. decreases from 290 to 210 at 0.1 Mrad and 309 rads/min. However, this effect is sensitive to dose rate and total dose. For example, at 1-10% NVP, but at
25 a lower dose rate of 64 rads/min., the mol. wt. increases from 400,000 to 4,590,000 and the C.A. decreases from 490 to 180.

In general, monomer concentrations in the range of 0.1-50% are preferred depending on other parameters.
30 Concentrations as low as 0.1 to 0.5% at low dose rates can yield hydrophilic surface grafts with C.A. below 30-40° under conditions of this invention. At monomer concentrations greater than 20-30%, effective grafting without solution polymer gelation requires low doses

and use of free radical scavengers. Monomer concentrations greater than 50% are feasible but not preferred since high concentrations of radical scavengers must be used and polymer mol. wts. and monomer conversion are lowered significantly by their use. For producing PHEMA coatings, HEMA concentrations of between 0.5% and 10%, by weight, are sufficient.

(b) Dose: In general, increasing total gamma dose increases mol. wt. of the polymer and reduces C.A. However, an important practical limit exists in that at higher doses, lower dose rates, and higher monomer concentrations, reaction media becomes extremely viscous or form gels which are very difficult to wash and to remove (e.g., about 0.25 Mrad and 10% NVP at 309 rads/min).

It will be understood by those skilled in the art that electron beam radiation will also induce graft polymerization. Therefore, electron beam radiation of energies equivalent to that described herein for gamma radiation may be substituted for gamma radiation in the practice of the method of the invention. Electron beam voltages in the range of from about 50 KeV to about 10 MeV may be employed at currents of from about 5 mA to about 100 mA. For electron beam initiated polymerization grafting, conditions which produce dose rates substantially higher than for gamma graft polymerization, i.e., in the range of from about 10 to about 10^8 rads/min or more may be employed.

(c) Dose rate: Decreasing gamma radiation dose rate generally increases solution PVP M.W., e.g., from 1,150,000 to 5,090,000 at 10% NVP and 0.1 Mrad as dose rate decreases from 1235 to 49 rads/min. The C.A. also goes down at lower dose rates, i.e., from 31° to 15°. As noted above, dose rates of up to 10^8 rads/min or

more are practical when employing electron beam irradiation.

(d) Solution Polymer Mol. Wt.: The mol. wt. may vary widely depending upon process conditions, monomers and radical inhibitors used. Effective grafting with low C.A. may therefore be achieved with even low mol. wt. solution polymer (M_v as low as 5000-10,000). However, solution polymer M_v greater than 5,000,000 or gels which form during grafting are generally impractical because of washing problems.

(e) Degassing: Removal of oxygen from the graft solutions by vacuum and/or inert gas (e.g., argon purging) has an important effect: lower total doses are required (practical grafting at less than 0.1 Mrad). Oxygen degassing also has a large effect on PVP M_v and % conversion of monomer. For example, with degassing, good grafting of PVP on polypropylene (PP) is achieved at 0.05 Mrad and 10% NVP (C.A. 15°). Without degassing, little grafting occurs under these conditions. Oxygen degassing is critical to hydrophilic surface modification grafting where the substrate polymer is PP, PVDF or PSI. It has been found that graft polymerization is inefficient when using these materials as substrates in the presence of oxygen. Oxygen degassing is also beneficial for PMMA and PC substrates in that much lower radiation doses (0.01-0.15 Mrad) become effective compared with grafting these polymers in the presence of oxygen.

f) Graft thickness: Surface grafts less than 100-200 Å, although non-adhesive and hydrophilic, are useful but may exhibit somewhat less mechanical "softness" or compliant gel-like surfaces than thicker coatings for reduced tissue-contact trauma. Graft coatings greater than ca. 300-500 Å (or 0.03 - 0.05 microns) up to 50 microns or more are probably more

desirable for many applications as long as they are smooth, uniform, optically clear for optic surfaces, and quickly hydrated.

Using no swelling solvents and no prolonged monomer
5 contact with substrates prior to irradiation, surface grafts which exhibit desired implant properties under preferred process conditions have thicknesses of about 0.1 to 5 microns. However, using swelling solvents such as ethyl acetate, polymer grafts on PMMA of 100
10 microns or more can be prepared.

For certain applications it may be preferred to have thicker "spongy" coatings of 20-100 microns.

g) Free-Radical Scavengers: Free radical traps, usually reducing agents such as Cu^+ , Fe^{+2} ascorbic
15 acid, etc, are known to inhibit radical polymerization in solution and thus be effective (especially at high gamma doses, high dose rates and high monomer concentrations) in slowing the onset of solution gelation during grafting. However, under practical grafting
20 conditions, this may result in lower mol. wts., high concentrations of unreacted monomer, and broad mol. wt. distributions. Use of metal salts may also be objectionable where maximum biocompatibility is critical.

25 Although most preferred graft conditions avoid the use of radical scavengers, useful conditions for graft coatings of PVP, P(NVP-HEMA) or PHEMA have also been defined using ascorbic acid to limit high viscosity and gelation of the graft polymer solution. These
30 conditions use high monomer concentrations (up to 50%) and thicker grafts are obtained using ethyl acetate as a swelling solvent (0.5-5%).

(h) Swelling solvents: The use of substrate
polymer solvents in the aqueous monomer grafting
35 solution facilitates swelling and monomer diffusion

into the polymer before and during gamma polymerization. Penetration of monomers into the substrate increases graft coating thickness and enhances bonding to the surface. Solvents such as ethyl acetate have
5 been shown to greatly facilitate this process with some substrates such as PMMA.

Although the above-described method represents a significant improvement over prior art methods, optimum results in each case depend upon the selection of a
10 combination of numerous process parameters and conditions.

Where mixtures of NVP and HEMA are employed to form graft copolymerized coatings of P(NVP-HEMA), the mixtures may contain up to about 50%, by weight, of
15 HEMA, based on the weight of the monomer mixture. However, above 20-30% HEMA, radical scavengers and low monomer concentrations should be used to prevent gelation since HEMA enhances the onset of gelation.

It will be understood by those skilled in the art
20 that the PVP, P(NVP-HEMA) or PHEMA graft coatings of this invention may be modified by copolymerization with various ionic monomers including use of such monomers for the presoak step. Mixtures of non-ionic hydrophilic monomers and ionic monomers may also be
25 copolymerized therewith. For example, graft copolymerization incorporating vinylsulfonic acid, styrene sulfonic acid, sulfoethylmethacrylate, sulfopropylmethacrylate or other vinyl sulfonic acids or vinylcarboxylic acids such as acrylic acid, crotonic acid or
30 methacrylic acid can afford surface modifications which are anionic. Similarly, graft copolymerization incorporating basic or amino-functional monomers, e.g., vinylpyridines, aminostyrenes, aminoacrylates or aminomethacrylates such as dimethylaminoethylmeth-
35 acrylate or dimethylaminostyrenes afford surface

modifications which are cationic. It is also useful to use salts of ionic monomers or to convert ionic grafts to the salt form by post-treatment.

Amounts of ionic monomers up to about 50 wt. % of the total monomer weight may be employed, it being understood that the critical process parameters listed above may be maintained.

In general, choice of the "best" process will depend upon molecular structure of the substrate and grafting polymer and the coating thickness desired. In general, those conditions which produce extreme solution viscosities and gels or conditions which could produce solvent stress cracking or crazing of the IOL polymers should be avoided. By way of example, the following process conditions are representative of practical conditions for the preparation of improved PVP grafts on various polymer substrates according to this invention.

Based on the foregoing considerations and the many process studies conducted, preferred conditions for various article substrate polymers by way of example are provided in the examples below. Some key points may be summarized as follows:

Several ranges of process conditions appear useful. Choice of the "best" process will depend on such factors as: molecular structure of substrate and coating thickness desired. In general, those conditions which produce extreme solution viscosities and gels or conditions which could produce solvent stress cracking or crazing of the IOL polymers (e.g., higher conc. than about 20% for a PMMA swelling solvent such as ethyl acetate) should be avoided. The following four sets of process conditions appear most practical for the preparation of improved surface modified ocular implants.

- (1) Aqueous Monomer Concentration: 5-20%
(preferred 10%)
Dose: 0.05-0.20 Mrad (preferred 0.10)
Dose Rate: 20-15,000 rads/min. (preferred
5 50-2,000)
C.A.: <30°
PVP M.W.: >250,000.
- (2) Same as (1) except that system is oxygen
degassed (vacuum or inert gas purge, e.g.,
10 argon) with
Dose: 0.01-0.15 Mrad (0.05 preferred) and
% NVP: 1-15% (5-10% preferred). This system
is generally preferred to (1).
- (3) Same as (1) and (2) with swelling solvent
15 (e.g., ethyl acetate for PMMA) gives greater
monomer penetration of substrate and thicker
grafts.
- (4) High monomer concentrations (25-50%) using
20 <5.0% ethyl acetate swelling agent and radical
inhibitor such as ascorbic acid (0.1-1.0mM) at
0.10-0.20 Mrad and 20-5000 rads/min.

All percentages expressed in the following non-limiting examples are by weight unless otherwise stated.

- 25 All contact angles (C.A.) and other surface
characterizations for gamma polymerization grafts,
unless otherwise indicated, are for samples washed with
water or water-alcohol at room temperature or elevated
temperatures to remove soluble residual monomer and
30 ungrafted polymer for the improved surface graft
processes of this invention. The resulting graft
polymers are stable and permanent for long-term ocular
implants and are not dissolved by aqueous media.

- 35 It will also be understood by those skilled in the
art that the instruments, devices, etc., to be graft

coated may be also constructed of materials other than PMMA, PP, PVDF, PC or PSi to facilitate their use. It will be understood by those skilled in the art that such materials may also be at least partially graft
5 polymer surface modified so as to improve their properties.

EXAMPLE 1

This example illustrates the important effects which result from varying the above-discussed process
10 conditions and polymerization parameters for gamma-irradiated polymer graft surface modification of PMMA with PVP.

PMMA slab samples were washed twice each by soap solution and distilled water using a sonicator. After
15 complete drying the samples were put into NVP solutions in glass vials. The samples were then γ -irradiated at various conditions. After γ -irradiation, the surface modified PMMA samples were rinsed several times with H₂O and evaluated.

20 The polymerized NVP grafting solutions or gels were freeze-dried under a vacuum. The solution PVP samples were evaluated for molecular weight by viscosity measurement (M_v) or gel permeation chromatography (M_w). For M_v , PVP was dissolved in distilled water and
25 intrinsic viscosity (IV), was measured at 30°C in a capillary viscometer.

PVP grafted PMMA samples were evaluated by water drop or underwater air bubble contact angle measurements. The bubble technique is regarded as more
30 reliable for very hydrophilic surfaces. For air bubble C.A., the grafted PMMA was held horizontally in distilled water. An approximately 0.8 μ l air bubble was formed and positioned underneath the test surface. Angles on opposite sides of the bubble were measured

assuring symmetry. Five measurements were usually made for each sample. The results are set forth in the following tables:

TABLE 1

5 Dose Rate Effect on Solution Polymer
 Molecular Weight For γ -Polymerized NVP

Concentration: 10% NVP in H₂O
 Total Dose: 0.1 Mrad

10	Distance from CO source	Dose Rate (rads/min)	Time (hrs.min)	[η]	Mol. Wt. (M_v) ($\times 10^6$)
	2"	1235	1.21	1.48	1.15
15	4"	309	5.24	2.21	2.27
	6"	137	12.09	2.61	3.04
	8"	77	21.36	2.85	3.49
	10"	49	33.45	3.56	5.09

20 The effect of dose rate was evaluated by PVP
 solution viscosity measurements. These results show
 that the molecular weight increased as dose rate
 decreased due to the slower and reduced initiation of
 radicals and the increased time of polymerization while
 25 maintaining the same total absorbed dose. At the
 lowest dose rate in this experiment, 49 rads/min (at
 10" from the Cobalt-60 gamma source) the highest
 molecular weight PVP polymer, $M_v = 5.09 \times 10^6$, was
 obtained.

25

TABLE 2Total Dose Effect on Molecular Weight γ -Polymerized NVPConcentration: 10% NVP in H₂O5 Dose Rate: 309 rads/min (4" from γ -source)

	Total Dose (Mrads)	Time (hrs.min)	[η]	Mol. Wt. (M_v) ($\times 10^6$)
10	0.05	2.42	1.86	1.69
	0.10	5.24	2.21	2.27
	0.25	13.30	*	---
	0.50	27.00	*	---
15	* Polymer solution gelled.			

Table 2 shows the effect of total irradiation dose on molecular weight at 309 rads/min. Increasing the total dose gives a higher molecular weight. A polymer gel was formed at a dose of 0.25 Mrad and higher.

20 These results show that high irradiation dose can cause gelation or cross-linking of the PVP polymer.

TABLE 3

Molecular Weight of γ -Polymerized NVP at
Different Solution Concentrations

Total Dose: 0.1 Mrad
Dose Rate: 309 rads/min.
 γ -Irradiation time: 5 hrs. 24 mins.

10	NVP Concentration		Mol. Wt. (M_v) ($\times 10^6$)
	(%)	[η]	
	3	0.97	0.56
	6	1.58	1.29
	10	1.94	1.82
15	15	2.45	2.70

20 These results show the relation between the concentration of NVP monomer and the molecular weights of PVP at constant dose and dose rate. The results indicate that higher NVP concentrations give higher molecular weight polymers. The importance of dose rate is also indicated by the fact that even at 15% NVP, the PVP molecular weight (M_v) was only 2.7×10^6 at 309 rads/min. compared to 5.0×10^6 at a lower dose rate of 49 rads/min.

TABLE 4

Contact Angle of PVP γ -Grafted PMMA
at Different Dose Rates

Concentration: 10% NVP

5 Total dose: 0.1 Mrad

	Distance from γ -source	Dose Rate (rads/min)	Time (hrs.min)	Contact Angle
10	Ungrafted PMMA control	---	---	65°
	PVP Grafted PMMA			
15	2"	1235	1.21	31°
	4"	309	5.24	24°
	6"	137	12.09	21°
	8"	77	21.36	19°
	10"	49	33.45	15°
20				

The results in Table 4 show that the contact angles for PVP grafted PMMA decreased due to hydrophilic PVP grafting and that the lower dose rates give lower contact angles.

TABLE 5

Contact Angle of PVP γ -Grafted PMMA
at Different Total Doses

Concentration: 10% NVP in H₂O

Dose Rate: 309 rads/min.

5

10

15

Total Dose
(Mrads)

Contact Angle

Ungrafted PMMA Control

65°

Grafted PMMA

0.05

27°

0.10

25°

0.25*

24°

0.50*

24°

*

Polymer solution gelled.

20

These results show the effect of total dose on the contact angles of PVP-grafted PMMA. The contact angle showed little change above 0.05 Mrad at constant dose rate of 309 rads/min.

TABLE 6

Contact Angle of PVP γ -Grafted PMMA
at Different Monomer Concentrations

Total Dose: 0.1 Mrad

Dose Rate: 309 rads/min.

5

NVP Concentration (%)		Contact Angle
10	Ungrafted PMMA Control	65°
	Grafted PMMA	
	3	29°
	6	27°
	10	25°
15	15	21°

The effect of different monomer concentrations was evaluated for PVP grafts on PMMA by contact angle measurement. Even at 3% NVP and 0.1 Mrad, a major increase in hydrophilicity was observed as compared with non-grafted PMMA. The contact angle decreased slightly at monomer concentrations above 3%.

20

TABLE 7

Molecular Weight of γ -Polymerized PVP
at Different Monomer Concentrations

5 Total Dose: 0.1 Mrad
 Dose Rate: 64 rads/min.

	NVP Concentration		Mol. Wt. (M_v) ($\times 10^6$)
	(%)	[η]	
10	1	0.79	0.40
	3	1.65	1.38
	5	2.23	2.30
	10	3.35	4.59

15 These results show the relationship between the
 concentration of NVP monomer and molecular weight of
 PVP at a dose rate of 64 rads/min.

 The molecular weight of PVP increases significantly
 with increasing concentration of NVP monomer.

TABLE 8

Contact Angle of PVP γ -Grafted PMMA
at Different Monomer Concentrations

Total Dose: 0.1 Mrad
Dose Rate: 64 rads/min.

5

	NVP Concentration (%)	Mol. Wt. (M_v) ($\times 10^6$)
10	Ungrafted PMMA Control	65°
	Grafted PMMA	
	0	62°
	1	49°
	3	43°
15	5	31°
	10	18°

The contact angle of PMMA was evaluated after γ -grafting with NVP at different solution concentrations at a dose rate of 64 rads/min. These results show that the contact angles of PVP-grafted PMMA decreased with increasing concentration of NVP monomer. This result, at 64 rads/min dose rate is qualitatively similar to results at 309 rads/min (Table 6). Hydrophilicity at 10% monomer appears to be favored somewhat by the lower dose rate (C.A. 18° vs. 25°).

Polar organic solvents or aqueous-polar organic solvent mixtures may be useful for hydrophilic monomer graft polymerization. Typical of such organic solvents are alcohols or ethers such as methanol, ethylene glycol, polyethylene glycols, dioxane, etc. However, when such organic solvents act as radical traps or radical chain transfer agents, they must be used at concentrations lower than 50% or with high hydrophilic monomer concentrations (i.e., >25%). For example,

methanol has some radical scavenger properties but may be used for PVP gamma grafts on PMMA in water-methanol mixtures up to 50-60% methanol for PVP grafts on PMMA using 0.1 Mrad and 10% monomer (Table 9). Hydrophilic grafts result although radical chain transfer by methanol appears to require low dose rates at 10% monomer. In general, these systems yield low viscosity solutions indicative of low molecular weight solution polymer which forms in the presence of radical inhibitors.

TABLE 9

Contact Angle of PVP γ -Grafted PMMA at Different Dose Rates in 50% Methanol (MeOH) Solution

Concentration: 10% NVP in 50% MeOH
Total Dose: 0.1 Mrad

	Dose Rate (rads/min)	Contact Angle
20	No graft	65°
	1065	36°
	326	28°
	157	27°
	64	20°

25

EXAMPLE 2

This example illustrates the effect of swelling solvents on the surface modification process.

For hydrophilic gamma grafts on PMMA as the substrate, for example, addition of the swelling solvent, ethyl acetate (EtOAc), to aqueous monomer solutions is advantageous to achieve more efficient

diffusion of monomer into the PMMA surface. Although EtOAc is not very soluble in water, a homogenous reaction medium can be achieved in the presence of a monomer such as NVP.

5 The thickness of the graft polymer surface modification can be increased by higher ethyl acetate concentrations and by longer diffusion times prior to irradiation; i.e., the time of pre-swelling. In general, without oxygen degassing, gamma radiation
10 doses of 0.10 - 0.15 Mrad are suitable to achieve significant amounts of grafting.

 The NVP-ethyl acetate-water solvent system is also a solvent for PVP and keeps the solution polymer phase homogenous.

15 "Embedded grafting" of PVP into the PMMA surface is made possible by irradiating the PMMA after exposure for various times to the monomer-swelling solvent-water mixture.

 In experiments using this process techniques,
20 samples were cleaned by sonication in a 10% soap solution followed by washing with distilled water. Prior to surface modification, PMMA samples were dried for 18 hours in a vacuum desiccator and weighed. NVP monomer was purified by vacuum distillation and stored
25 at 4°C.

 For gamma radiation grafting, the PMMA substrate was immersed in aqueous monomer-solvent solutions and exposed to gamma radiation. Typically, cleaned substrates were immersed in NVP-ethyl acetate-H₂
30 mixtures and irradiated in a 600 Curie Co-60 source. The samples were exposed to the monomer solution for various lengths of time. Gamma doses ranging from 0.01 - 0.15 Mrad as measured by Fricke dosimetry were used in this experiment. Dose rates were also varied.
35 After irradiation, samples were removed from the gamma

polymer solution and washed several times with distilled water and in deionized water with agitation. Some samples were weighed hydrated after blotting with filter paper to remove surface water and then dried for 24 hours in a vacuum desiccator. The polymerization solutions ranged from clear viscous solutions to gels. The following parameters were measured.

One measure of the degree of grafting was obtained from the weight increase of the substrate according to the following equation:

$$\text{percent grafting} = \frac{W_1 - W_0}{W_0} \times 100$$

where W_0 is the initial weight of PMMA and W_1 is the weight of grafted PMMA. Likewise, percent hydration was calculated according to the following equation:

$$\text{percent hydration} = \frac{W_w - W_d}{W_d} \times 100$$

where W_w is the weight of PMMA after equilibration in water (after blotting it dry) and W_d is the weight of dry sample (after desiccation). In most cases, the maximum water uptake was reached after 12 hours.

Captive air bubble and n-octane contact angles were measured for the radiation grafted PMMA surfaces to estimate the hydrophilicity of modified surfaces. Static contact angles were measured on a Rame-Hart contact angle goniometer. At least five measurements on different surface regions of each sample were made. IR/ATR surface analysis of the grafted and ungrafted surfaces was made by using a Perkin-Elmer Model 283B IR Spectrometer using attenuated total reflectance.

Samples of 1cm^2 grafted and ungrafted PMMA were analyzed using a Kratos ES 300 ESCA spectrometer employing a magnesium K α x-ray source. Graft analysis consisted of N/C ratio determination.

The molecular weights of PVP solution polymers were determined by solution intrinsic viscosity measurements at 30°C in a Ubbelohde viscometer.

Radiation doses ranged from 0.01 to 0.15 Mrad and monomer concentrations ranged from 5 to 15%.

Data for PVP grafting onto PMMA using EtOAc as a swelling solvent are shown in Table 10. Since no pre-radiation swelling time is used here, diffusion penetration of the surface by EtOAc and monomer occurs during gamma radiation. Some pre-radiation swell-time is considered preferable. This system exhibits behavior typical of a reaction which involves monomer diffusion control. Partitioning of NVP monomer into the hydrophobic surface of PMMA is favored initially because of the presence of the ethyl acetate, which is a swelling solvent for PMMA.

By the use of a swelling solvent for the graft substrate (i.e., EtOAc), the NVP-EtOAc-H₂ system swells the surface layers of PMMA and polymerization grafting of monomer molecules in the vicinity of radiation induced radical species near the surface is immediate. Under such conditions, more efficient grafting is achieved at lower doses and with deeper penetration of the graft polymer into the solvent swollen surface.

Measurement of percent swelling of PMMA samples in NVP-ethyl acetate-H₂O (1:1:8) vs. time shows that swelling of about 6% is attained after 12 hours. In this system, the thickness of the grafted layer could be controlled by changing the time allowed for diffusion prior to irradiation, thus controlling the thickness of the grafted zone. Table 11 shows the graft behavior after 24 hours of pre-swelling of PMMA in 1:9 ethyl acetate: water containing 15% of NVP. Comparing this data with Table 10 (no swelling time), it is clear that the % graft is significantly higher

for pre-swelling PMMA. At a given ethyl acetate concentration, this difference is generally more pronounced at lower monomer concentrations, e.g., 5% monomer compared to 15% monomer.

5 In this system, NVP is the monomer but also acts as a mutual solvent to maintain a homogeneous phase of otherwise poorly miscible solvents, i.e., ethyl acetate and water. At a given monomer concentration (e.g., 10%), it is necessary to keep the concentration of
10 ethyl acetate below 10% to avoid phase separation to a micro-emulsion. Variation of the ethyl acetate concentration, being a swelling agent, affects graft yield. Table 12 summarizes the observations made by varying the concentration of ethyl acetate while
15 keeping other factors constant showing that the percent grafting does increase with higher ethyl acetate concentrations. Greater grafting efficiency is also indicated by the significant % grafting and reduction of C.A. in the solvent swelling monomer system at low
20 doses. For example, up to 0.05 Mrad, little grafting occurs in a simple aqueous monomer system. In contrast, at only 0.01 Mrad C.A. is reduced to 35° (Table 11, 24 hr. pre-swell) and to 23° at 0.03 Mrad.

 Techniques used for the chemical analysis of bulk
25 polymers are usually not very satisfactory for analysis of the surfaces of polymers. The surface region, which is significantly different in structure and/or chemistry from the bulk, is present only as a fraction of the mass of the polymer. Thus, the traditional
30 techniques of chemical analysis are inadequate. Special surface analysis techniques are required for graft copolymers since the surface region is a complex mixture of graft, substrate, cross-linking groups and chain transfer products. Two spectroscopic methods,
35 ATR-IR and ESCA are the most useful methods now

available for this purpose and were used to help characterize grafted surfaces.

The results for ATR-IR (attenuated total reflection infrared) shown in Table 13 indicate that the ration of
5 C=O (ester) and C=O (amide) groups in the surface changes from 7.67 to 1.68 as the gamma dose increases from 0.01 to 0.10 Mrad and then levels off which is consistent with PVP grafting on PMMA.

ESCA analyses are shown in Table 14 and indicate
10 increasing nitrogen composition with increasing dose (and grafting) as expected for a PVP graft.

Scanning electron microscopic examinations of the grafted samples were performed in order to observe their surface morphologies. All of the coated surfaces
15 appeared smooth even at 10,000X. The graft polymer surface modifications appear to provide uniform coverage across the surface of PMMA substrate. This is important to insure excellent retention of optical properties for an optical implant such as an intra-
20 ocular lens.

Major conclusions to be drawn from the results of this example are:

The NVP-ethyl acetate-water system produces uniform hydrophilic graft polymer surfaces with controllable
25 graft penetration using PMMA as the substrate.

The monomer-ethyl acetate-water grafting front gradually penetrates into the substrate and may be controlled by varying the concentration of swelling agent and the time of pre-swelling.

30 The presence of the PVP surface graft was confirmed by gravimetric, contact angle, ATR-IR and ESCA measurements.

Unusually low radiation doses are required to achieve significant grafting. Hence, any possible
35 radiation damage to the surface or substrate is minimized.

38

TABLE 10

Graft Polymerization of NVP on PMMA

Swelling time - 0 hours

Ethyl acetate : H₂O (1:9)

Dose Rate (rads/min)	NVP Conc.	<u>0.01 Mrad</u>		<u>0.05 Mrad</u>		<u>0.10 Mrad</u>		<u>0.15 Mrad</u>	
		C.A.	% Graft	C.A.	% Graft	C.A.	% Graft	C.A.	% Graft
309	5%	48	--	47	0.5	42	0.7	36	0.7
	10%	46	0.1	34	0.4	22	--	17	0.5
	15%	40	0.2	32	0.5	16	0.9	18	0.5
77	5%	40	0.2	38	0.2	41	0.6	38	0.3
	10%	36	0.6	32	0.4	35	0.7	36	0.5
	15%	38	1.1	25	0.5	28	0.8	26	0.6

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TABLE 11

Grafting of NVP on PMMA: 24 Hours Swelling

Solvent - 9:1/H₂O-EtOAc/NVP - 15%

Total Dose (Mrads)	309 rads/min		77 rads/min		3 g
	C.A.	% Graft	C.A.	% Graft	
0.01	38	1.0	35	1.3	
0.03	27	2.3	23	2.8	
0.05	17	2.5	17	2.4	
0.10	16	3.0	16	3.2	
0.15	10	3.0	16	3.4	

SECRET

TABLE 12

Graft Polymerization of NVP on PMMA
 Effect of Ethyl Acetate : 12 hours Swelling
 10% NVP, 309 rads/min

Total dose (Mrads)	3% EtOAc		6% EtOAc		10% EtOAc	
	C.A.	% Graft	C.A.	% Graft	C.A.	% Graft
0.01	43	0.2	44	0.4	48	0.6
0.03	38	0.3	26	0.5	25	1.7
0.05	23	0.3	21	0.5	22	1.9
0.10	18	0.5	17	0.5	18	2.2
0.15	15	0.5	17	0.6	18	2.2

41

TABLE 13ATR-IR Spectral Analysis of PVP-Grafted PMMA Samples*

5	Total Dose (Mrad)	$v_C = 0$ (ester)
		$v_C = 0$ (amide)
	0.01	7.67
	0.03	6.51
10	0.07	4.61
	0.10	1.68
	0.15	1.66

15 * Reaction mixture 5% NVP in 9:1 mixture of water-ethyl acetate, dose rate 1065 rads/min - Swelling time: 17 hours.

TABLE 14ESCA Analysis of PVP Grafted PMMA Samples*

20	Total Dose (Mrad)	N/C at 0°C
	0.03	2.2×10^{-2}
	0.05	3.1×10^{-2}
	0.07	4.5×10^{-2}
25	0.10	4.7×10^{-2}

* Reaction mixture - 5% NVP in 9:1 mixture of water-ethyl acetate. Dose rate 1065 rads/min - Swelling time: 17 hours.

EXAMPLE 3

30 The following experiment demonstrates the very significant influence of oxygen on gamma polymerization and gamma grafting and the important beneficial effects

of carrying out graft polymerizations in the substantial absence of oxygen.

Gamma radiation induced polymerization of NVP was carried out in 10% NVP aqueous solution as follows:

- 5 (a) polymerization in presence of oxygen (air);
- (b) polymerization in absence of oxygen using argon degassing; and
- (c) polymerization in absence of oxygen.

For Group (a), aqueous 10% NVP solutions were
10 irradiated to total doses of 0.01, 0.05, 0.10, 0.20 and 0.25 Mrad in each case at 213 rads/min in the presence of air. An argon purge for 10 minutes was used in the case of (b). A vacuum freeze-thaw (FT) method was
15 employed for degassing in the case of Group (c). In the freeze-thaw experiments, the monomer solution was frozen in liquid nitrogen and then vacuum (0.3 mm) was applied to eliminate oxygen. The frozen solution was thawed and brought to room temperature before irradiation. Some samples were subjected to three freeze-thaw
20 cycles (3 FT). Experiments were run in duplicate to establish reproducibility.

To determine the oxygen degassing effects on gamma radiation grafting and polymerization, monomer conversions and molecular weights were determined for
25 the different NVP solutions irradiated at 0.01 Mrad to 0.25 Mrad at 213 rads/min.

A method used for determining unreacted NVP after irradiation was as follows: 5 ml of the gamma irradiated NVP solution was extracted using 50 l
30 acetonitrile. NVP is soluble in acetonitrile but PVP is not. The PVP precipitate was centrifuged and the supernatant solution was analyzed for NVP. The NVP monomer solution (10% NVP/aqueous) was used as a control. NVP analysis was as follows: The 10% by
35 weight aqueous solution was diluted with acetonitrile

to appropriate concentrations (0.5 g/ml to 5.0 g/ml). The U.V. absorbance was measured for each solution at 323 nm to develop a standard curve of NVP concentration vs. U.V. absorbance. The regression coefficient was 0.99 for this curve. GPC was used for molecular weight measurements and gives M_w as well as molecular weight distribution.

The % NVP conversion (amount of monomer reacted) is significantly affected by Ar purge deoxygenation and by FT oxygen degassing. At the very low dose of 0.01 Mrad, virtually no polymerization occurs in the non-degassed oxygen (air) containing solutions. However, 46%, 61% and 63% conversion to PVP occurred for the AR-purged, 1 FT and 3 FT samples, respectively. Even at 0.10 Mrad, samples irradiated in air showed only 90% conversion (10% unreacted NVP monomer) compared to virtually complete conversion (99%) for oxygen degassed systems. This is important for biological implants where unreacted monomers can cause serious adverse toxicological behavior.

To demonstrate more efficient grafting of PVP on PMMA at low gamma doses in the oxygen degassed system, 10% aqueous NVP was argon purged to remove oxygen and irradiated with PMMA samples at 157 rads/min to 0.05 Mrad. The resulting hydrophilic surface modification had C.A. 20° and was stable (no change in C.A.) to mechanical abrasion. As indicated above, this mechanically stable and very hydrophilic graft of PVP on PMMA graft is achieved with high monomer conversion (98%) and a high degree of polymerization for the solution polymer (1.65×10^6 mol. wt.). In the presence of air (oxygen), higher radiation doses (>0.1 Mrad) and/or higher monomer concentration (15% or more) are required to achieve low C.A. with high conversion and high molecular weight. For hydrophilic monomer

gamma polymerization grafts on other substrate polymers, i.e., polypropylene, fluorocarbons (e.g., PTFE or PVDF), or silicones, the beneficial effect of oxygen degassing can be even greater. Oxygen removal
5 may also be used for improved gamma grafting in combination with the use of substrate swelling solvents and free radical inhibiting agents such as oxidizable metal salts or organic compounds (e.g., ascorbic acid). In the presence of radical inhibitors effective
10 grafting may be achieved but solution polymer may be of low mol. wt.

PVP molecular weight is also greatly affected by oxygen degassing. The Ar-purged and FT samples yield PVP polymers with molecular weights of about 1.6×10^6
15 at only 0.01 Mrad. In sharp contrast, the non-degassed samples do not form high mol. wt. polymer. At 0.05 Mrad, oxygen degassed samples yield PVP with molecular weights of $1.65 - 1.8 \times 10^6$ compared with only about 0.35×10^6 in air. At 0.10 Mrad, all samples have
20 molecular weights of about 1.8 to 2.0×10^6 .

EXAMPLE 4

The following experiments were carried out to demonstrate the advantageous effects of free radical scavengers in inhibiting solution polymerization and
25 gelation during the graft polymerization process, especially at high monomer concentrations.

PMMA samples were surface grafted with PVP using gamma irradiation as in Example 1. Ascorbic acid (AsCA) was used as a radical inhibitor in these
30 experiments. The irradiation conditions are set forth in Table 15.

TABLE 15

- a) 30% NVP/0.5mM AsCA/2.5%EtoAc/0.2 Mrad*
b) 30% NVP/0.5mM AsCA/2.5%EtoAc/0.15 Mrad
c) 40% NVP/1.0mM AsCA/0.1 Mrad
5 d) 50% NVP/1.0mM AsCA/0.1 Mrad
e) 50% NVP/1.0mM AsCA/0.2 Mrad*
* 0.1 Mrad initial dose; additional 0.1 Mrad after
washing sample free of monomer and soluble polymer.

10 C.A. for all PMMA samples in Table 15 were 18-24°
indicating very high hydrophilic grafts. Dose rates
used were 33 rads/min. A dose rate of 667 rads/min for
(b) was also used. Solution polymer gelation can occur
under these conditions at these monomer concentrations
(30-50%) if a radical inhibitor such as AsCA is not
15 used. The AsCA significantly inhibits solution
polymerization without interfering with grafting
yielding low mol. wt. solution polymer. In addition to
C.A., PVP grafting was verified by ESCA and FTIR-ATR
analysis showing the presence of surface nitrogen and
20 the PVP imide carbonyl group. Good mechanical
properties were demonstrated by an abrasion test
showing little change in C.A. or surface nitrogen after
abrasion.

EXAMPLE 5

25 This example demonstrates the large favorable
effect of hydrophilic gamma graft surface modification
on reducing tissue adhesion by measuring corneal
endothelium adhesion and cell adhesion using fibroblast
cells. These are important factors in demonstrating
30 the improved biocompatibility and minimal tissue
irritation or damage afforded by the hydrophilic graft
surface modifications of this invention.

An apparatus which measures the force of adhesion (mg/cm^2) between contacting polymer and tissue surfaces was used to determine adhesion between rabbit corneal endothelium and polymer surfaces. Adhesion force values of about 250-400 mg/cm^2 were measured for PMMA and other hydrophobic polymers evaluated for implants, i.e., silicone, polypropylene, etc. The improved hydrophilic gamma graft surfaces, prepared under preferred process conditions, exhibit much lower adhesion; below 150 mg/cm^2 and often less than 100 mg/cm^2 . This is accompanied by a major reduction in endothelium cell damage as measured by SEM; from about 50-80% damage for PMMA or silicone to 20% or less for surfaces gamma grafted under preferred process conditions of this invention.

The gamma graft surface modifications of this invention also show a major reduction in cell adhesion as demonstrated by exposure to live cell cultures of chick embryo fibroblast cells (CEF) or rabbit lens epithelial cells (LE). Experiments indicate that 2-4 times more CEF or LE cells adhere to PMMA as compared to PVP graft modified PMMA. Grafts prepared at 0.1 Mrad and using 15% NVP, for example, showed adherence of only 35% of the number of CEF cells which adhere to PMMA. Similarly, PHEMA grafts on PMMA exhibited only 38% cell adhesion and 15:1 NVP:HEMA (at 16% total monomer) exhibited only 20% CEF cell adhesion compared to PMMA. Under optimal conditions of the method of the invention for PVP surface modified PMMA, PC or PSi, less than 1-2 LE cells per sq. mm. adhere as compared to about 10 LE cells or more to unmodified PMMA, PC or PSi.

EXAMPLE 6

This example demonstrates the graft polymerization of HEMA and mixtures of NVP and HEMA on PMMA.

The method of Example 1 was repeated utilizing a
5 16% NVP/HEMA (15:1) aqueous solution at about 1300
rads/min and 0.10 Mrad dose. The PVP-PHEMA surface
modified PMMA had a C.A. of 17°. Under similar
conditions, a 7% NVP/HEMA solution (5:2) gave a surface
with C.A. 23°, and a 2.5% HEMA solution gave a surface
10 with C.A. 18°.

EXAMPLE 7

This example demonstrates the graft copolymeriza-
tion of anionic or cationic monomers with the hydro-
philic monomers of this invention using ionic monomers
15 with NVP.

a. The method of Example 1 was used with PMMA
substrate and 15% NVP plus 1-5 wt% of acrylic acid (AA)
or crotonic acid (CA) as comonomers at 0.1 Mrad and
1235 rads/min. Contact angles were 18-22° and
20 endothelium adhesion was about one half or less that of
unmodified PMMA indicating formation of a good
hydrophilic graft coating. Similar results can be
obtained using dimethylaminoethylacrylate to produce
cationic graft coatings. Styrene sulfonic acid (SSA)
25 was also used to produce anionic grafts with NVP on
PMMA according to the method of Example 1. Using an
SSA:NVP ratio of 1:2 (33% SSA) and total monomer
concentration of 30% at 0.15 Mrad and about 700
rads/min dose rate, hydrophilic grafts with 30-40° C.A.
30 were prepared.

b. Styrene sulfonic acid sodium salt (NaSSA) was
used to prepare highly hydrophilic anionic copolymer
grafts with NVP on silicones (PDMS). PDMS samples were
cleaned by sonication in ethanol and vacuum dried prior

to irradiation in aqueous monomer solutions. Table 16 lists grafting conditions, monomer concentrations and contact angles for graft surfaces prepared at a dose rate of about 700 rads/min.

5

TABLE 16

	<u>Dose</u> <u>(Mrad)</u>	<u>% NaSSA</u>	<u>% NVP</u>	<u>C.A.</u>
	0.05	20	20	17°
	0.10	20	20	15°
10	0.15	20	20	13°

As shown in Table 16, under conditions of even a relatively low total dose of 0.05 Mrad, using 40% total monomer and 50% anionic NaSSA comonomer with NVP, very hydrophilic (C.A. 17°) anionic grafts were achieved.

15

EXAMPLE 8

This example demonstrates the hydrophilic monomer surface grafting of polypropylene (PP) and the importance of oxygen degassing for effective surface modification.

20

Hydrophilic surface grafts on polypropylene are not readily prepared by gamma irradiation of aqueous NVP in the presence of oxygen. Under conditions of Example 1, even at gamma doses >0.1 Mrad and monomer concentrations >10%, little surface hydrophilicity and little reduction in C.A. occurs. However, in oxygen degassed media, at 157 rad/min, and doses as low as 0.01-0.05 Mrad with 10% NVP, contact angles were about 15°. Very hydrophilic PP grafts which are also mechanically stable by a mechanical abrasion test are thereby readily prepared using oxygen degassed process conditions. This is especially important for gamma

25

30

graft surface modification of IOLs with PMMA optics and PP haptics.

EXAMPLE 9

5 Surface modification of polycarbonate is most readily accomplished using gamma radiation of oxygen degassed aqueous monomer NVP solutions, e.g., grafting conditions of oxygen degassed 10% NVP at 93 rad/min and 0.05 Mrad dose yield C.A. 19°.

EXAMPLE 10

10 Although silicone (PSi) does not gamma graft with NVP as readily as PMMA, PSi surfaces were modified using oxygen degassed 10% NVP solutions. Irradiation to 0.05 Mrad at 93 rad/min yields C.A. of about 45° indicating significant surface hydrophilicity. Higher
15 doses, swelling solvents, higher monomer concentrations and different hydrophilic monomers can produce improved hydrophilicity. For example, gamma grafting of NVP/HEMA (10:1) at 0.10 Mrad and 157 rad/min even without oxygen degassing yields grafts with 30° C.A.

EXAMPLE 11

20 Polyvinylidene fluoride (PVDF) is an example of a fluorocarbon polymer which can be surface modified by gamma irradiation of aqueous NVP, NVP/water-methanol solutions or EtOAc-water systems. Hydrophilic grafts,
25 with C.A. about 30°, are prepared at 326 rad/min and 0.20 Mrad. However, PVDF is preferably grafted using oxygen degassed process conditions. Conditions of 157 rad/min, 0.05 Mrad, and 10% aqueous NVP produce PVP grafts with C.A. 17°. Since NVP monomer is also an
30 effective swelling solvent for PVDF, allowing pre-radiation swelling time is favorable for producing improved grafts. For example, C.A. as low as 14° is

obtained using 5 hrs. swelling time with 7% NVP, 0.10 Mrad and 94 rads/min.

EXAMPLE 12

Hydrophilic Surface Modification of FEP Teflon

5 Intravenous Catheter Polymers by PVP and PVP/HEMA

FEP teflon is a fluorocarbon polymer which is used for a number of medical devices such as intravenous catheters. It is very hydrophobic with a contact angle greater than 95° and shows significant tissue adhesion and damage on contact as indicated by in vitro rabbit
10 corneal endothelium tests: about 250 mg/cm² adhesion force and 30-50% cells destroyed. FEP teflon film was surface modified by the following procedure to produce hydrophilic surfaces with contact angles less than 30-
15 40°, with tissue adhesion reduced to less than about 120 mg/cm², and tissue damage reduced to less than 20%. For example, FEP films immersed in 25% aqueous NVP monomer and irradiated to gamma doses 0.10 and 0.25 Mrad (without oxygen degassing) yield hydrophilic PVP
20 graft surfaces with contact angles of 33° and 26°, respectively. The endothelium adhesion force was 45 mg/cm² for the latter sample and FTIR-ATR spectroscopy verified the presence of the PVP surface graft. FEP intravenous catheters exhibit improved surface
25 properties when hydrophilic surface modified by the materials and processes of this invention; i.e., reduced pain and insertion force, reduced vascular endothelium damage, improved blood compatibility and reduced susceptibility to adherence of pathogens and
30 associated infections. Central venous catheters and heart catheters are also beneficially surface modified in this manner. Other fluorocarbon polymer catheters (e.g., PTFE) are similarly improved by this hydrophilic surface modification.

A further improvement in the γ -graft process for hydrophilic surface modification of fluorocarbon polymers is achieved through a surface pre-treatment with a defluorinating agent such as sodium naphthalene. For example, exposure of PTFE to a sodium naphthalene solution for only 30-60 seconds followed by γ -grafting of PVP or HEMA resulted in grafts with improved wettability as compared with no pre-treatment and contact angles of 18° for 10% aqueous NVP and 0.1 Mrad, 22° for 1% HEMA and 0.005 Mrad, and 19° for 10% NVP/HEMA and 0.01 Mrad.

EXAMPLE 13

Hydrophilic Surface Modification of Porous PTFE Vascular Graft (GoretexTM) by γ -PVP Process

Porous PTFE vascular grafts are presoaked in acetone, acetone-water-monomer solutions and then irradiated immersed in an aqueous monomer solution; typically 10% NVP, 5% acetone, 85% water in a gamma source to 0.02 - 0.15 Mrad total dose. After thorough washing with water, the PTFE was characterized and shown to have a hydrophilic surface modification by a major reduction in contact angle (from 98° unmodified to about 20° for the PVP surface graft). The PVP surface modification is also shown by FTIR-ATR surface spectroscopy. The mechanical properties of the fluorocarbon polymer substrate are virtually unchanged by the very low gamma radiation doses required for hydrophilic polymer grafting. The surface modification is shown to have little effect upon the porous structure of the PTFE vascular graft by scanning electron microscopy.

The resulting hydrophilic surface modified PTFE and porous vascular graft materials exhibit improved blood compatibility properties of special value for small

diameter vascular grafts and for other blood contacting implants and devices, i.e., heart valves, ventricular assists, artificial hearts, vascular catheters and pacer leads.

5 The very low doses of this invention do not damage or change the bulk properties of PTFE substrates and the use of low gamma doses with aqueous polymerization media results in very thin uniform hydrophilic surface modifications with retention of the substrate structure
10 and physical properties, i.e., the pore structure of porous vascular graft PTFE materials.

EXAMPLE 14

NVP-HEMA Copolymer Gamma Grafting on FEP Teflon

NVP-HEMA copolymer gamma-grafting of FEP teflon was
15 found to be very efficient at NVP:HEMA ratios of 9:1 and 8:2 yielding very hydrophilic surface modification with 10% aqueous monomer solutions and 0.1 Mrad (contact angles of 30° or less). At 8:2 NVP:HEMA and 10% monomer, contact angles less than 30° can be
20 achieved at less than 0.05 Mrad. Hydrophilic surface modified FEP teflon intravenous catheters are readily prepared by this method to yield catheters with reduced insertion force and pain, and which are less likely to exhibit i.v. catheter complications such as
25 infection, phlebitis, clotting, etc.

EXAMPLE 15

Surface Modification of Polyurethanes

Polyurethanes (PUR) have become increasingly important polymers for medical devices and implants,
30 especially for i.v. catheters, pacer leads, vascular grafts and artificial heart applications. Although PURs are generally more hydrophilic than silicones or fluorocarbons, they do not generally exhibit the

significant reduction in tissue adhesion and low tissue damage properties of more hydrophilic graft polymer surface modifications, i.e., PVP gamma grafts.

5 Improved surface properties for medical devices and implants are achieved by the gamma-irradiation surface modification process of this invention.

For example, films of a 55 durometer polyurethane polyether block copolymer (Pellthane 5363) were gamma irradiated to 0.1 Mrad in oxygen degassed 10% aqueous
10 NVP to yield significantly more hydrophilic surfaces. The unmodified contact angle of 54° was reduced to 28° for the PVP surface modified PUR. In vitro endothelium contact damage tests for PURs yield cell damage results averaging 60% or more compared to cell damage of less
15 than 20% which is found for the hydrophilic PVP surface modifications. This improvement in PUR surface properties is especially important for commonly used radio-opaque PUR formulations containing such additives as barium sulfate because such formulations tend to
20 have poorer biocompatibility. A typical PUR (Pellthane) formulation containing about 12% BaSO₄, for example, exhibits very high endothelium contact damage (80%) which is greatly reduced (<30%) by hydrophilic polymer surface modification.

TABLE 17

Some Tissue Damage Data Using In Vitro
Rabbit Endothelium Contact Testing
For Different Polymers Compared to
Hydrophilic PVP Gamma-Grafts

5

	<u>Contact</u> <u>Angle</u>	<u>Endothelial</u> <u>Cell Damage</u>
PMMA	65-72°	60-80%
FEP		
10 Fluorocarbon	95-105°	30-50%
Silicone	90-100°	60-80%
Gamma-PVP on PMMA		< 20%
Gamma-PVP on Silicone		< 20%
Gamma-PVP on FEP fluorocarbon		< 20%

15 It is conventional for many medical device polymers
to be filled with barium or bismuth radio-opaque
compounds (i.e., BaSO₄) to enable X-ray examination.
This can make surfaces even more damaging to tissues.
Surface modification according to the method of the
20 present invention is especially beneficial for such
radio-opaque polymer compositions to provide smoother,
tissue-protective, more biocompatible surfaces.

EXAMPLE 16Hydrophilic Surface Modified

25

PMMA Contact Lenses

This example illustrates the beneficial tissue-
protective properties obtained by hydrophilic polymer
surface modification of conventional hard (PMMA)
contact lenses. Such contact lenses are normally
30 irritating and abrasive to the external corneal
epithelium. PMMA contact lenses are surface modified
by gamma-graft polymerization immersed in aqueous NVP

monomer (typically 10% NVP) using 0.1 Mrad dose. The resulting transparent hydrophilic graft makes the contact lens surface water wettable ($<30^\circ$ C.A.) and non-adherent to the epithelial surface, thereby
5 reducing epithelial abrasion and irritation. The various process improvements of this invention may be readily adapted to produce contact lenses with controlled surface modification thickness suited to specific patient needs.

10

EXAMPLE 17Hydrophilic Surface ModifiedSilicone Soft Contact Lens

Silicone soft contact lenses are widely used due to their mechanical flexibility and good oxygen permeability. However, silicone is normally hydrophobic.
15 It is, therefore, not water wettable and may adhere to or abrade sensitive corneal epithelial tissue. Many types of silicone contact lenses are surface-treated with an oxidizing plasma to increase water wettability and minimize this problem. However, this type of
20 surface oxidation has only a slight tissue-protective value and is usually transient in aqueous media. The silicone surface loses its hydrophilicity and becomes less wettable, often within a few weeks. In contrast,
25 the hydrophilic polymer surface grafts of this invention are permanently bound chemically and persist indefinitely to maintain excellent water wettability. Furthermore, they exhibit non-adherent, lubricious, tissue-protective qualities in contact with the corneal
30 epithelium, thereby minimizing abrasion and irritation while retaining the favorable optical, mechanical and oxygen permeability properties of the polysiloxane.

EXAMPLE 18Hydrophilic Surface ModifiedEndotracheal Tubes and Cuffs

Endotracheal and tracheostomy tubes are convention-
5 ally made of silicones, polyurethanes, fluorocarbon
polymers and polyvinyl chlorides. Balloons or cuffs on
these airway devices are inflated during intubation and
are usually made of latex rubber, vinyl or silicone
polymers. Significant clinical problems associated
10 with the use of these devices are desquamation of the
ciliated cells of the trachea and even more severe
damage to the trachea due to the pressure, irritation
and adhesion of the cuffs. Post-operative infections
are associated with adherence of pathogens to the
15 damaged and denuded areas of the trachea caused by the
airway tube cuffs. Hydrophilic polymer surface
modification of the tube and cuff surfaces according to
this invention affords a significant improvement in
these devices by minimizing abrasive contacts and
20 adhesion to the sensitive tracheal tissues.

A silicone cuff is modified with PVP-PHEMA (10:1)
by the methods of Example 10. The resulting hydro-
philic cuff has markedly reduced adhesion to tissue and
causes less tracheal irritation and damage than
25 hydrophobic polysiloxane cuffs. Similarly, a latex
rubber cuff is modified with gamma-grafted PVP
according to the method of Example 8. The resulting
hydrophilic cuff is less adherent to sensitive tracheal
tissue than normal hydrophobic latex rubber cuffs
30 causing less tracheal irritation and damage during
intubation.

EXAMPLE 19Hydrophilic Surface Modification of
Foley Catheter Tubes and Balloons

Foley catheter tubes and balloons are used for
5 catheterization of the urinary tract and conventionally
made of the same hydrophobic polymers used for endo-
tracheal tubes and cuffs as noted in Example 18.
Clinical complications associated with such devices are
tissue irritation, infection and encrustation due to
10 the tissue adherent and damaging surface properties of
the hydrophobic catheters and the adherence of patho-
gens, proteins and minerals to the surfaces. Although
silicone and fluorocarbon polymers tend to exhibit
reduced mineral deposits and encrustation, hydrophilic
15 polymer surface modification affords improved resis-
tance to the problems of tissue irritation, infection
and encrustation.

A silicone Foley catheter is modified with PVP-
PHEMA (10:1) according to the methods of Example 10.
20 The resulting hydrophilic surface modified catheter has
reduced tissue adhesion and exhibits less encrustation
than unmodified silicone. In another example of the
advantages of this invention, a Foley catheter with a
latex balloon is surface modified according to the
25 method of Example 8 yielding a hydrophilic surface
which is less likely to promote infection and is less
susceptible to encrustation.

EXAMPLE 20Hydrophilic Surface Modification of
Surgical Gloves and Sponges

30 Latex rubber surgical gloves exhibit hydrophobic
surface properties and tend to adhere to sensitive
tissue surfaces thereby enhancing manipulative damage
to tissues in all types of surgery. Manipulative

damage can result in increased post-operative complications such as infection and surgical adhesions. Hydrophilic surface modification of surgical gloves results in reduced tissue adhesion of the rubber latex and less chance of severe manipulative tissue trauma due to contact with gloves. Latex rubber gloves are surface modified with a hydrophilic PVP surface according to the method of Example 8. The very low gamma-dose required by the process of this invention makes it feasible to accomplish this hydrophilic polymer grafting without altering the mechanical properties of the radiation-sensitive rubber latex. The resulting hydrophilic latex surgical gloves are less adherent and less damaging to sensitive tissue normally contacted during surgery, i.e., peritoneum, pericardium, etc.

Surgical sponges and gauzes used in surgical procedures are also damaging to tissue due to tissue adhesion and abrasion. Sponges and gauzes are normally made of cotton, polyesters, cellulosic material and polyurethanes. These natural and synthetic polymers are all amenable to hydrophilic surface modification by the materials and processes of this invention. In a typical example, a cotton gauze sponge is surface modified by gamma-grafting with PVP using 10% aqueous NVP and 0.1 Mrad dose. The sponge surface is thereby rendered more hydrophilic and less abrasive to tissue during surgical manipulation without altering the structure and function of the sponge.

30

EXAMPLE 21

Hydrophilic Surface Modification of Silicone Mammary Prosthesis

Mammary prostheses are most commonly constructed of a hydrophobic polysiloxane skin or membrane containing

air, water or silicone gels or fluids. A major complication of such soft tissue prostheses is the irritation and inflammatory process which occurs at the tissue-implant interface which leads to formation of a hard fibrous capsule surrounding the implant. This fibrous capsule can severely compromise the bio-acceptance of the prosthesis and, if severe, can lead to tissue necrosis, extrusion and loss of the implant. The hydrophilic surface modification of the silicone which is accomplished by this invention leads to reduced tissue irritation and abrasion by the implant and reduced adhesion of infiltrating cells during the postoperative period which normally can lead to extensive fibrous capsule formation. A silicone bag/silicone gel mammary prosthesis is surface modified with a hydrophilic PVP-PHEMA graft according to the method of Example 10. This hydrophilic prosthesis surface is less adherent to tissue or cells as compared to normal silicone and thereby has improved bio-compatibility with less tendency to form a surrounding hard fibrous capsule.

EXAMPLE 22

Hydrophilic Surface Modification of Carbon Fiber Composite Reinforced Polycarbonate Surgical Instrument

Plastic surgical instruments made of various hydrophobic structural polymers are used to an increasing extent because plastics lend themselves to high quality - low cost manufacture of special value for disposable instruments. Such instruments may exhibit significant tissue adhesion with accompanying manipulative trauma. Improved tissue-protective properties are achieved by the hydrophilic polymer surface modification of this invention. Fiber

reinforced composites are among the most important examples of plastic materials used for instruments (containing glass, carbon or boron fibers to provide rigidity and high mechanical strength). A carbon fiber reinforced bisphenol-A polycarbonate microsurgical forcep for surgical insertion of an ocular implant is an example of a surgical instrument which is significantly improved by this invention. Using the process of Example 9 for the polycarbonate polymer, the carbon fiber reinforced polycarbonate instrument is readily surface modified with PVP. The resulting instrument surface is much less adherent to tissue and less damaging in contacts with fragile ocular tissues. Additionally, the surface modified plastic instrument is less likely to scratch or damage the surface of plastic ocular implants.

EXAMPLE 23

Hydrophilic Surface Modification of Silicone

Irrigation/Aspiration (I/A) Tools

Used in Ophthalmic Surgery

In ophthalmic surgery, I/A tools are used to irrigate the eye with irrigating solutions and to aspirate fluids and tissue debris out of the eye. Silicone tips are commonly used on such I/A instruments. They are maneuvered around the anterior and posterior chambers of the eye with resulting frequent contacts with fragile tissues. For hydrophobic silicone devices, these tissue contacts may cause significant tissue damage which can compromise the success of the ocular surgery.

Silicone I/A tips are surface modified with PVP and PVP-PHEMA by the process of Example 10. The resulting hydrophilic polymer surface is less adherent to tissue

and less damaging on contact with sensitive tissues during surgery.

EXAMPLE 24

Hydrophilic Surface Modification of Polyurethane Artificial Heart

5 Implants or ex-vivo heart assist and artificial heart devices are most often constructed of woven fiber reinforced segmented polyether polyurethanes because of their superior mechanical strength properties.

10 However, these materials are still thrombogenic to a significant degree and clotting complications severely limit the use of such devices. Modification of the surfaces of such devices with hydrophilic polymer grafts which are less thrombogenic by virtue of low

15 blood cell and platelet adhesion and activation, low fibrinogen adsorption, etc., is efficacious in prolonging the useful life of such devices and implants. A polyurethane Jarvic-7-type artificial heart is readily surface modified with a FVP graft by

20 the process of Example 15. This process is uniquely suitable for the uniform hydrophilic surface modification of highly irregular complex structures such as the artificial heart since the entire device is immersed in the monomer solution and radiation permeates the entire

25 structure to uniformly activate the substrate and initiate surface graft polymerization in a controlled manner.

EXAMPLE 25

Hydrophilic Surface Modification of Polyvinylchloride (PVC) Catheters

30 PVC is widely used for catheters, blood tubing, blood bags and many other medical devices. Formulations are hydrophobic and exhibit some adverse tissue

adhesion and cell adhesion behavior. Hydrophilic surface modification is useful in improving blood and tissue compatibility. Since formulations often contain significant concentrations of plasticizers (i.e., dioctyl phthalate), leaching of surface plasticizer by washing with appropriate solvents such as aqueous acetone prior to gamma graft surface modification is preferred. After aqueous acetone washing, a PVC vascular catheter is exposed to 0.1 Mrad immersed in degassed 10% aqueous NVP to yield a hydrophilic PVP graft which exhibits less vascular endothelium damage on contact and which is less thrombogenic than unmodified PVC.

EXAMPLE 26

Hydrophilic Grafting of Medical Devices Having Combinations of Materials

One of the important aspects of this invention is the discovery that certain grafting process conditions make it feasible to surface modify combinations of materials to be used in medical devices. Surface grafting of an assembled device can then take place in a one-step simultaneous grafting procedure yielding improved, more biocompatible surfaces. Material combinations of PMMA, PC, PUR, fluorocarbons, PP, PSi and other polymers can thereby be grafted under conditions of this invention. Table 18 summarizes some device combinations with preferred mutual grafting conditions for obtaining improved PVP grafts.

PMMA/PP and PMMA/PVDF

It has been demonstrated that PMMA and PP gamma graft under degassed conditions at 157 rad/min, 0.05 Mrad, 10% NVP. These conditions yield contact angles of 20° and 15° for PMMA and PP, respectively, and are mechanically stable. Non-degassed PP does not graft

efficiently under conditions similar to PMMA because of the adverse effect oxygen has on PP surface grafting.

- 5 PVDF surface graft studies also indicate the importance of oxygen degassing. A 10% degassed aqueous NVP solution, irradiated at 157 rad/min to 0.05 Mrad, gives good hydrophilic grafts on both PMMA and PVDF. See Table 17.

PC/PP and PC/PVDF

- 10 PC and PP graft under similar gamma irradiation conditions when NVP solutions are degassed. Using 157 rad/min, 0.05 Mrad, and 10% aqueous NVP solutions, efficient hydrophilic grafting occurs on both polymers yielding contact angles of 19° and 15°, respectively.

TABLE 18
Surface Modification of Medical Device
Combinations with PVP

5	Polymer Combination	Typical Preferred Gamma Polymerization Grafting Conditions*
10	PMMA/PP	a. 10% degassed NVP, low dose rate (LDR)**, 0.05 Mrad. b. 2.5% EtOAc, 6 hr swell, 10% NVP, degassed LDR, 0.05 Mrad.
15	PMMA/PVDF	a. 10% degassed NVP, LDR, 0.05 Mrad. b. 10% NVP, 5 hr swell, LDR, degassed, 0.15 Mrad. c. 2.5% EtOAc, 6 hr swell, 10% NVP, degassed, LDR, 0.05 Mrad.
20	PC/PP	a. 10% degassed NVP, LDR, 0.05 Mrad. b. 2.5% EtOAc, 6 hr swell, 10% NVP, LDR, degassed.
25	PC/PVDF	a. 10% degassed NVP, LDR, 0.05 Mrad. b. 10% NVP, 5 hr swell, LDR, degassed, 0.05 Mrad. c. 2.5% EtOAc, 6 hr swell, 10% NVP, degassed, LDR, 0.05 Mrad.
30		

* To produce C.A. less than about 25°.

** LDR : 30-300 rads/min.

35

EXAMPLE 27

This example illustrates the efficient grafting which can be achieved by the process of this invention at extremely low gamma doses (0.005 Mrad or less) even at very low aqueous monomer concentrations (0.5 wt% or less).

40

PVDF surfaces were surface modified using conditions described in the above examples at the extremely low gamma-radiation doses (0.01 and 0.005 Mrad) and low HEMA monomer concentrations (0.5-2.0%) summarized in Table 19. PVDF samples were cleaned, gamma irradiated in aqueous HEMA solutions, and washed according to the general method of Example 1. Highly hydrophilic surface graft modifications are achieved as indicated by the low contact angles listed in Table 19. Good graft efficiency for PHEMA on PVDF under these extremely low dose and monomer concentration conditions is further confirmed by the XPS analyses given in Table 20 which shows little surface fluorine and a corresponding increase in carbon for the PHEMA-g-PVDF; a surface analysis which closely approximates the composition of PHEMA.

TABLE 19

Gamma Radiation Graft Polymerization of Argon
Degassed Aqueous HEMA on PVDF at 88 rads/min

20	Total Dose (Mrads)	% HEMA	Contact Angle (°)
		0.5	24
25	0.005	1.0	24
		2.0	12
		0.5	21
	0.01	1.0	19
		2.0	16

Even at doses as low as 0.005 Mrad or less and monomer concentrations as low as 0.5 wt% or less, extremely hydrophilic PHEMA grafts are obtained. For

comparison, PVDF itself is very hydrophobic and has a contact angle greater than 85°.

TABLE 20

XPS Analysis of PVDF and PHEMA-g-PVDF

5		C(1s)	F(1s)
		<u>Carbon</u>	<u>Fluorine</u>
	Unmodified PVDF	50.5	45.3
	PHEMA-g-PVDF		
	2% HEMA	69.0	0.9
10	<u>0.005 Mrad</u>		
	PVDF (theoretical)	50.0	50.0
	PHEMA (theoretical)	66.7	

The XPS surface analysis clearly shows that efficient surface grafting of PHEMA occurred at 0.005 Mrad. The surface carbon concentration for the graft was about that expected for a PHEMA surface and very little surface fluorine for PVDF was detected.

CLAIMS:

- 1 1. In a method for modifying a plastic surface of
2 an article, said surface adapted for contact with
3 living tissue of a human or non-human animal, by the
4 gamma-irradiation induced polymerized chemically
5 grafted coating thereon of:
6 1) a monomer comprising N-vinylpyrrolidone
7 (NVP),
8 2) a monomer comprising 2-hydroxyethyl-
9 methacrylate (HEMA),
10 3) a mixture of (NVP) and (HEMA), (NVP-
11 HEMA), or
12 4) a mixture of 1), 2) or 3) with up to
13 about 50 wt%, based on the total monomer weight, of an
14 ionic monomer, salt of an ionic monomer or mixture
15 thereof; so as to form a hydrophilic graft polymer
16 coating of:
17 I. polyvinylpyrrolidone (PVP),
18 II. poly-2-hydroxyethylmethacrylate (PHEMA),
19 III. a copolymer of (NVP) and (HEMA),
20 [P(NVP-HEMA)], or
21 IV. a copolymer of (NVP), (HEMA) or (NVP-
22 HEMA) and said ionic monomer, on said surface, the
23 improvement comprising:
24 conducting said gamma-irradiation induced
25 graft polymerization in an aqueous solution under the
26 following conditions:
27 a) monomer concentration in the range of
28 from about 0.1% to about 50%, by weight;
29 b) total gamma dose in the range of from
30 about 0.001 to less than about 0.50 Mrad; and
31 c) gamma dose rate in the range of from
32 about 10 to about 2500 rads/min.

- 1 2. The method of Claim 1 further including one or
2 more of the following conditions:
3 d) substantially excluding free oxygen from
4 said graft polymerization solution;
5 e) maintaining the thickness of said polymer
6 coating in the range of from about 100 Å to about 100
7 microns;
8 f) including a free radical scavenger in
9 said aqueous graft polymerization solution; and
10 g) including in said aqueous graft polymer-
11 ization solution a swelling solvent for said plastic
12 surface.
- 1 3. The method of Claim 1 wherein said article is
2 a surgical instrument.
- 1 4. The method of Claim 1 wherein said article is
2 a medical device.
- 1 5. The method of Claim 1 wherein said article is
2 a prosthetic implant.
- 1 6. The method of Claim 1 wherein said article is
2 a soft or hard contact lens.
- 1 7. The method of Claim 1 wherein said ionic
2 monomer is a vinylsulfonic acid, a vinylcarboxylic acid
3 or a salt thereof.
- 1 8. The method of Claim 7 wherein said vinylcar-
2 boxylic acid is acrylic, methacrylic or crotonic acid.

70

15 thereof; so as to form a hydrophilic graft polymer
16 coating of:

17 I. polyvinylpyrrolidone (PVP),

18 II. poly-2-hydroxyethylmethacrylate

19 (PHEMA),

20 III. a copolymer of (NVP) and (HEMA),

21 [P(NVP-HEMA)], or

22 IV. a copolymer of (NVP), (HEMA) or

23 (NVP-HEMA) and said ionic monomer, on said surface com-
24 prising:

25 conducting said electron beam-irradiation
26 induced graft polymerization in an aqueous solution
27 under the following conditions:

28 a) monomer concentration in the range of
29 from about 0.1% to about 50%, by weight;

30 b) total electron beam irradiation dose in
31 the range of from about 0.001 to less than about 0.50
32 Mrad; and

33 c) an electron beam irradiation dose rate in
34 the range of from about 10 to about 10^8 rads/min.

1 14. An article prepared according to the method of
2 Claim 1 or 13.

1 15. An article according to Claim 14 comprising a
2 surgical instrument, medical device, prosthetic implant
3 or contact lens.

INTERNATIONAL SEARCH REPORT

International Application No. PCT/US91/06730

I. CLASSIFICATION OF SUBJECT MATTER (if several classification symbols apply, indicate all) *		
According to International Patent Classification (IPC) or to both National Classification and IPC IPC(5) A01N 1/02; B05D 3/06 U.S. CL. 427/2,36 522/84,85,167 604/96 606/107 623/1,3,,66		
II. FIELDS SEARCHED		
Minimum Documentation Searched ⁷		
Classification System *	Classification Symbols	
U.S. CL.	427/2,36 522/84,85,167 604/96 606/107 623/1,3,66	
Documentation Searched other than Minimum Documentation to the Extent that such Documents are Included in the Fields Searched *		
III. DOCUMENTS CONSIDERED TO BE RELEVANT *		
Category *	Citation of Document, ¹¹ with indication, where appropriate, of the relevant passages ¹²	Relevant to Claim No. ¹³
X	US,A, 4,897,433 (SUGO et al.) 30 JANUARY 1990 see Entire document	1-15
&	US,A, 4,961,954 (GOLDBERG et al.) 09 OCTOBER 1990	
<p>* Special categories of cited documents: ¹⁰</p> <p>"A" document defining the general state of the art which is not considered to be of particular relevance</p> <p>"E" earlier document but published on or after the international filing date</p> <p>"L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)</p> <p>"O" document referring to an oral disclosure, use, exhibition or other means</p> <p>"P" document published prior to the international filing date but later than the priority date claimed</p> <p>"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention</p> <p>"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step</p> <p>"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art.</p> <p>"&" document member of the same patent family</p>		
IV. CERTIFICATION		
Date of the Actual Completion of the International Search	Date of Mailing of this International Search Report	
21 OCTOBER 1991	07 NOV 1991	
International Searching Authority	Signature of Authorized Officer	
ISA/US	MICHAEL R. LUSIGNAN	